



# Microdynamic Materials Properties of Composites for Space Applications

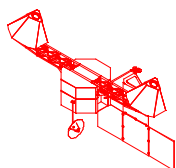
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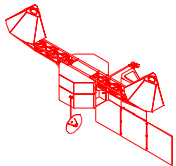


# Presentation Outline

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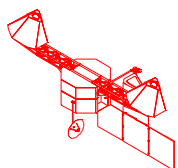
- **Materials Properties for Macro Damping**
  - Typical algorithms and terminology
  - Composites vs. metals
  - Parameters influencing macrodynamic materials properties
- **Toward Microdynamic Materials Properties**
  - Typical materials and properties for space applications
  - Some empirical and anecdotal information
  - Optimizing microdynamic performance
  - Screening test matrix for space materials
- **Microcracking as an Input Energy**
  - Microcracking explained /criteria
  - Space composites performance
  - Proposed experiments



# Damping Terminology



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Term	Symbol	Definition
% Critical Damping Factor	$c_c$	$c_c = 2 m \omega_p = 2 \sqrt{km}$
Viscous Damping (critical damping ratio)	$\zeta$	$\zeta = \frac{c}{2m\omega_p} = \frac{c}{c_c}$
Structural Damping	$g$	$g = \eta = \frac{1}{Q} = 2\zeta$
Loss Factor (loss tangent, $\tan\phi$ )	$\eta$	$\eta = 2\zeta$ <span style="margin-left: 20px;"><math>G^* = G(1 + i\eta)</math></span>
Quality Factor	$Q$	$Q = \frac{1}{\eta} = \frac{1}{2\zeta}$
Logarithmic Decay	$\delta$	$\zeta = \frac{\delta}{2\pi}$ where $\delta = \ln\left(\frac{x_1}{x_{1+1}}\right)$
Specific Damping Capacity		$= \frac{2}{Q} = 2\zeta = 4$

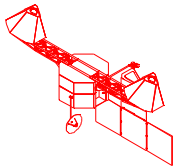


# Composite Materials Internal Damping Estimates

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- **Probable Micro-Models for Damping**
  - Microplastic or viscoelastic phenomena associated with matrix
  - Relative slippage at the fiber-matrix interface
- **Given: Matrix damping capacity & fiber/matrix moduli:**
  - Can estimate internal damping of composite with known  $V_f$
- **Typical levels for space structures**
  - = 0.5to 2% critical
  - Optical benches are lowest, integral, in-plane designs



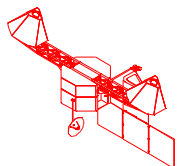
# Uni-Directional Lamina Damping Estimate



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Longitudinal Shear Specific Damping Capacity

$$_{LT} = \frac{m \left( (1 - V_f)(G + 1)^2 + V_f (G - 1)^2 \right)}{\left[ G \left( (1 + V_f) + 1 - V_f \right) \right] \left[ G \left( (1 - V_f) + 1 + V_f \right) \right]}$$

Longitudinal Tension/Compression Specific Damping Capacity

$$_L = m \left( (1 - V_f) \frac{E_m}{E_L} \right)$$

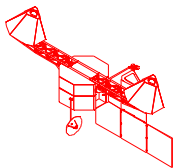
Where, based on rule of mixtures

$$E_L = E_f V_f + E_m (1 - V_f)$$

Transverse Specific Damping Capacity

$$T \quad m$$

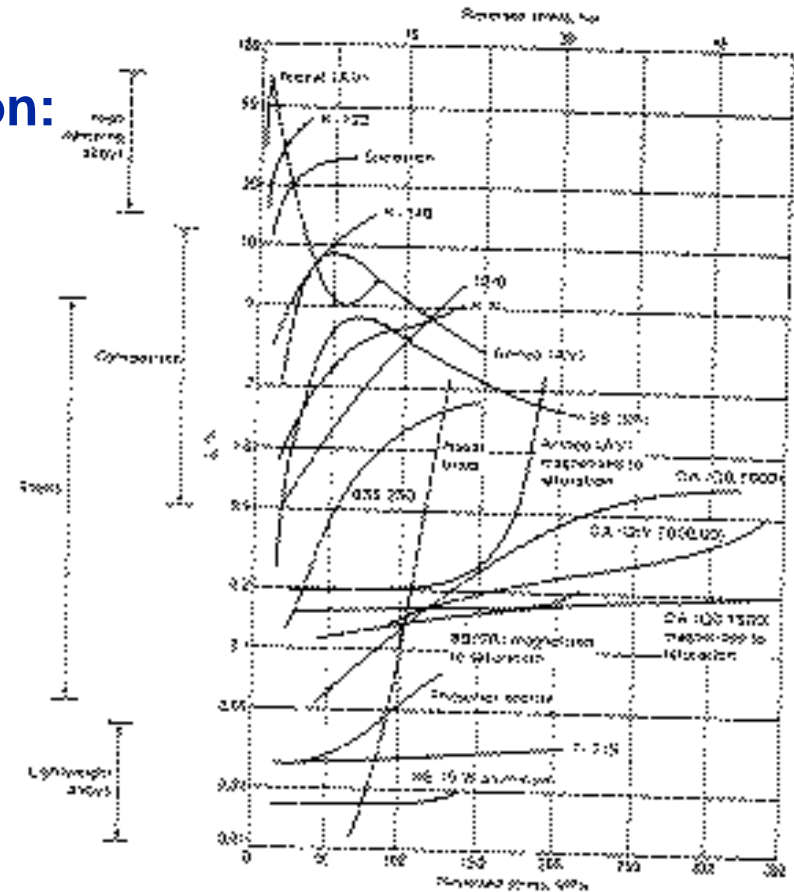
Laminate Damping Estimates	
<b>Fiber Properties</b>	
Name: T300	
Fiber Vol Fraction [%]:	55%
Fiber Longitudinal Modulus E <sub>f</sub> [Msi]:	33
Fiber Shear Modulus G <sub>f</sub> [Msi]:	3.2
<b>Matrix Properties</b>	
Name: 954-3	
Matrix Longitudinal Modulus E <sub>m</sub> [Msi]:	0.4
Matrix Shear Modulus G <sub>m</sub> [Msi]:	0.148
Matrix SDC <sub>m</sub> [%]:	15.00%
(SDC: Specific Damping Capacity)	
<b>Uni-Directional Lamina Damping Properties</b>	
Shear Modulus Ratio G =	21.622
Longitudinal Young's Modulus E <sub>L</sub> [Msi] =	18
(Based on rule of mixtures)	
Lamina Longitudinal Tension/Compression SDC <sub>L</sub> [%] =	0.15%
Lamina Longitudinal Shear SDC <sub>LT</sub> [%] =	13.14%
Lamina Transverse Tension/Compression SDC <sub>T</sub> [%] =	9.84%
<b>Longitudinal Tension/Compression</b>	
Lamina Critical Damping ratio [%] =	0.01%
Lamina Loss Factor =	0.02%
Lamina Quality Factor Q =	4266
<b>Longitudinal Shear</b>	
Lamina Critical Damping ratio [%] =	1.05%
Lamina Loss Factor =	2.09%
Lamina Quality Factor Q =	48
<b>Transverse Tension/Compression</b>	
Lamina Critical Damping ratio [%] =	0.78%
Lamina Loss Factor =	1.57%
Lamina Quality Factor Q =	64



# Composite Materials Damping



- **Composite material internal damping is highly dependent on:**
  - **Load levels (direct)**
  - **Loading frequency (direct)**
  - **Temperature (direct)**
  - **Composite Material:**
    - Moduli (extension, shear) (ind.)
    - Fiber volume fraction (ind.)
    - Ply orientation (thickness?)
  - **Fiber drives:**
    - Extensional moduli
  - **Resin drives:**
    - Shear and transverse moduli
    - Matrix damping capacity

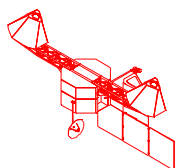




# Typical Composites for Space Structures



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- By Structural Type
- Basic Requirements
- Typical Fiber and Resin Constituents

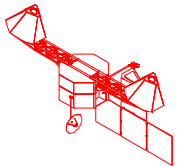
Structure Type	Requirements		Reinforcing Fibers Matrix Resin			
	Iso. Modulus (10E6 psi)	CTE (ppm/°C)	Outgas/CMEPAN- based	Pitch-based	Type	
1. Zero CTE Space	12 to 16	<±0.09	Very Low	M55J, M60J	P75, K135, K13710, XN50A	Cyanate
2. Stiff Structure	15 to 20	-3 to +4	NASA Spec	M55J, M60J	K135, XN50, K13710, K13C, P75	Epoxy or Cyanate
3. Aluminum Equivalent	>10	<23	NASA Spec	M40J, M46J	K63312	Epoxy
4. Fabric Skins / SAS3 (Kev)	3 to 40	±2	NASA Spec	M40J, M55J, M60J	XN50A, K13, K13C, XN70	Epoxy or Cyanate



# Internal Damping Performance of Space Composites



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- **Load levels**
  - Typically low (good)
- **Loading Frequencies**
  - Structural: first modes 4 to 150 Hz, ~low (bad)
  - Instrument: 100 to ? Hz for SIM, NGST, etc. (good?)
- **Composite Materials for Space**
  - High Stiffness: in-plane and on-axis (bad!)
  - Low Stiffness: transverse, shear moduli (good, but avoided)
  - Matrix Damping Capacity: epoxies, cyanates, VEMs (good)
  - Adhesives, Bonded Joints: continuous, but good damping

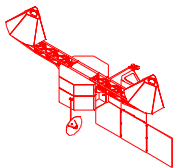




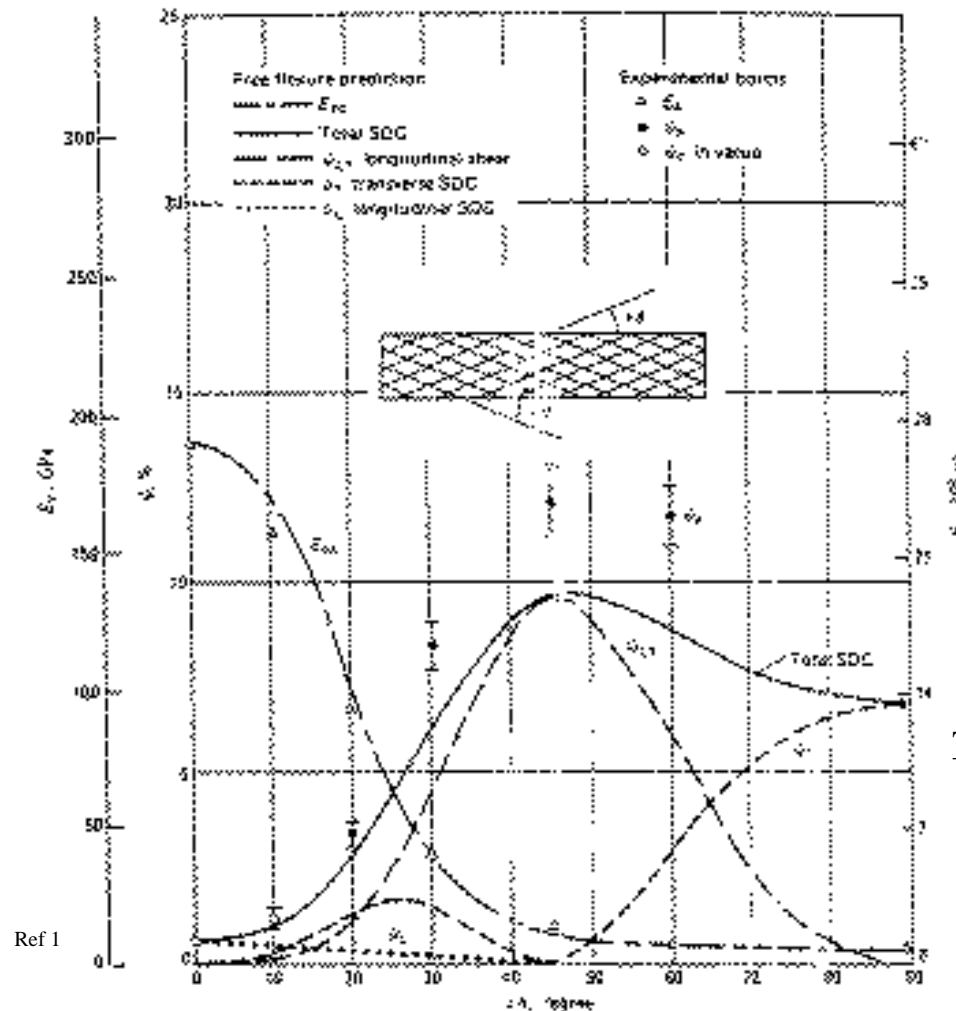
# Laminate Damping Variation w/ Ply Angle



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$$= \frac{1}{s_{11}} \frac{T}{E_T} \sin^4 + \frac{LT}{G_{LT}} \sin^2 \cos^2$$

Bias Plies +/- 45deg:

chart ? 10%

$$? = \frac{1}{4} = 0.008 \text{ or } 0.8\%$$

T300/954-3 [0/45/90/135] Laminate:

? 0.01 or 10%

T300/IM8 Hybrid [0<sub>n</sub>/+45/-45/0<sub>n</sub>/...] Laminate:

? 0.006 or 0.6%

Ref : Adams, Robert D., "Damping Properties Analysis of Composites", ASM International, Engineered Materials Handbook, Vol 1.

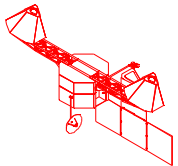


## Empirical Info on Composites Damping

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- **Pitch versus PAN**

- Several sporting goods references cite much better damping from pitch-based than PAN-based fibers of the same moduli
- Could be related to higher micro-strain levels in matrices around pitch fibers or to a difference in fiber damping capacity

- **Interlayers Work**

- Numerous references (AFRL SPICE program, others) have shown visco-elastic materials (VEMs) like polyurethanes, silicones do increase damping without hampering structural performance

- **Use Materials With Hysterisis**

- Early non-linearity in shear responses
- VEMs which can be engineered within the glass transition zone



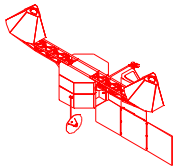
# Improving Space Composite Damping



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- **Extensional Moduli**
  - Use highly-off axis laminates
  - Consider lower modulus fibers (Carbon, Glass, Kevlar)
  - Design 'soft' boundaries / interfaces where possible
- **Shear and Transverse Moduli**
  - Use lower modulus resins (e.g. cyanate vs. epoxy)
- **Matrix Damping Capacity**
  - Choose resins with 'early' non-linear shear responses
  - Use interlaminar VEMs, or resin rich layers
  - Load resins with low E or high damping phases
- **Other**
  - Choose fibers with higher damping (pitch vs. PAN ?)
  - Use smaller ply thicknesses (more discreet interlaminar layers)



# Screening Matrix for Microdynamic Properties of Space Composites

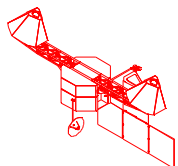
- Parametric Test Matrix
- Choose Parameters and # of Settings
  - Based on available budgets

Test Types	Test Conditions	Materials
	Type, Settings	Temps. Fibers Resins
Damping Ratio	High & Low on Freq. & Amp.	77 K, 300 K M55J (78), K13710 (90), T300 (33), K1100 (140), Kevlar Cyanate, Epoxy, Modifieds, VEM layers
Extensional Modulus	Uni TN or CM	
Shear Modulus	±45 TN, Iosipescu	
Transverse Modulus	90° TN or CM, FWT	
Fiber Volume	50% & 60%	

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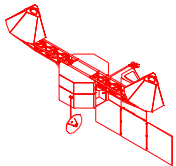
# Microcracking in Space Composites



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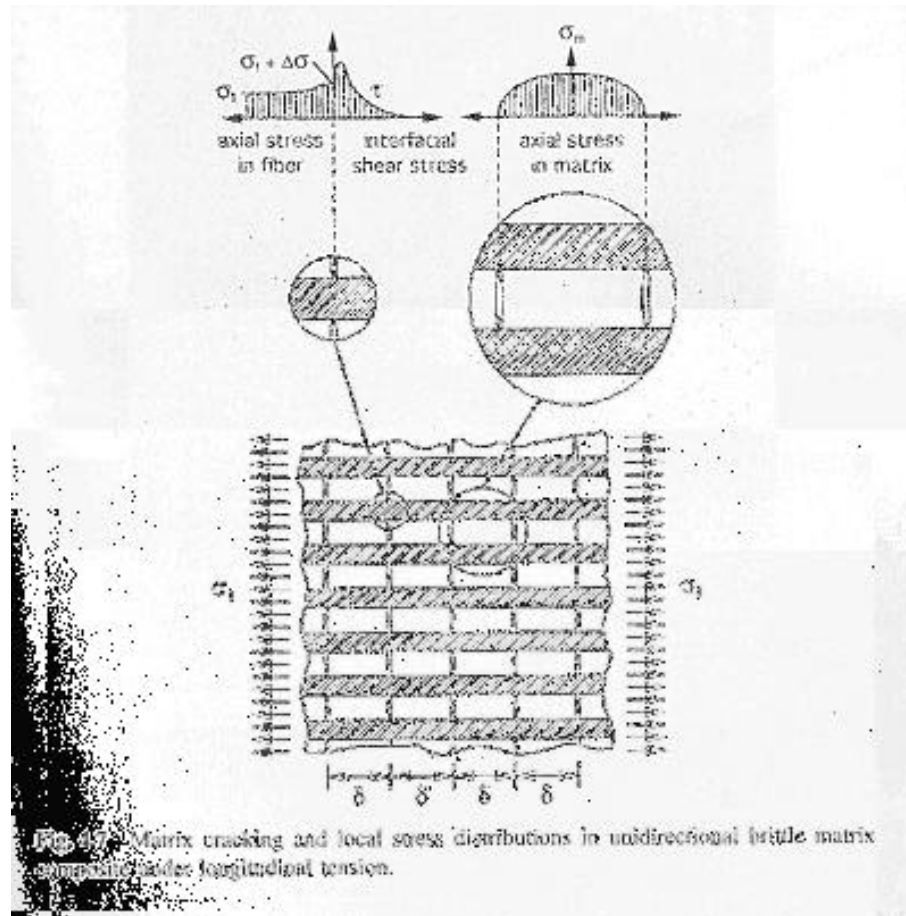
- **Will Probably Happen Due To:**
  - Temps below about  $-100^{\circ}\text{C}$
  - Zero CTE laminates have highly negative CTE fibers
  - Ply thicknesses typically 2.5 to 5 mils (64 to 127 microns)
  - Current resin properties: cyanates are better, but not that good.
- **Mitigating Techniques**
  - Layup orientations with gradual transition
    - I.e. (0,45,90, 135)XS better than (0, 90, +45, -45)XS
  - Thinner plies
    - 25 micron possible, but expensive and limits fiber choices
  - Higher strain matrices
    - Elastomer loading, high strain base resins
    - VEMs like polyurethane as interlaminar layers



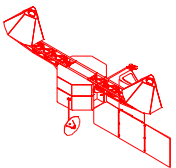
# Microcracking Micromechanics



- Negative CTE of neighboring plies adds to tensile thermal stress in resin on cool down until resin fails



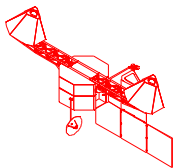
SIM



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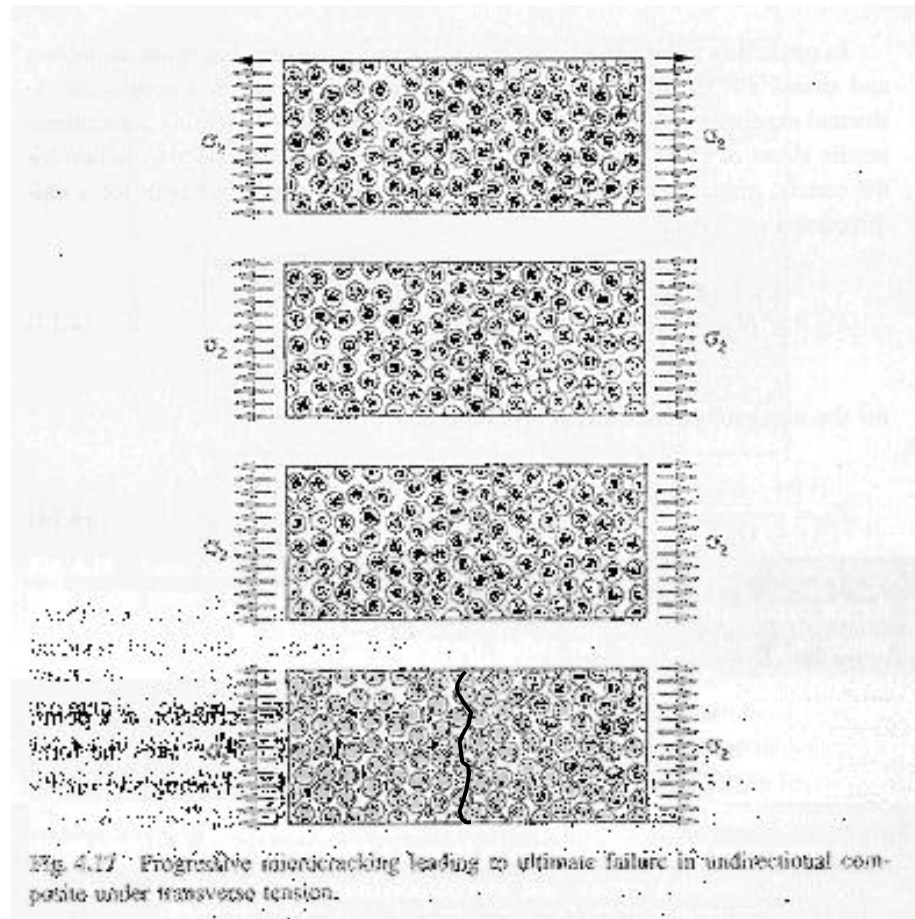
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# Microcracking Damage Progression

**cal**  
**JPL**



Ref : Daniel, Isaac M. and Ishai, Ori, "Engineering Mechanics of Composite Materials," p. 100

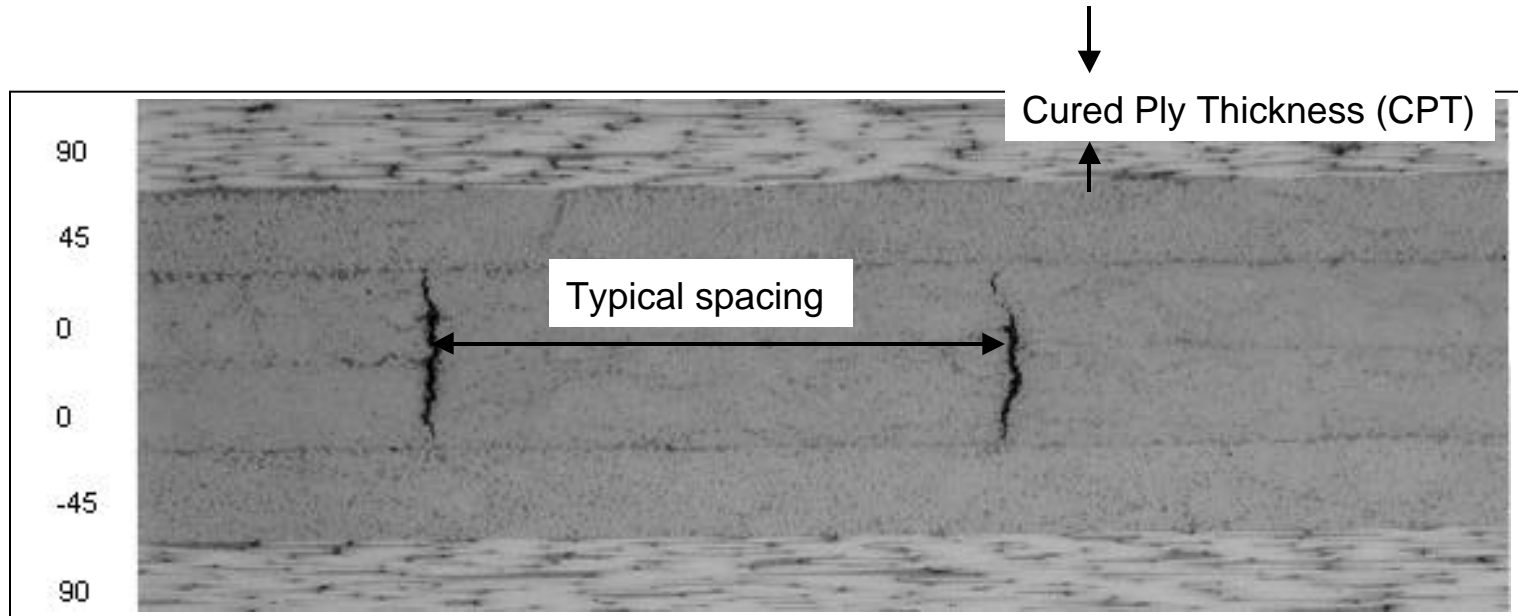




# Microcracking in a Space Composite



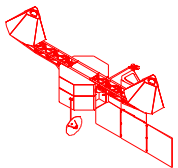
Ply  
Orientation



Resin Type / Ultimate Strain ( $\epsilon_{RESIN}^{ULT}$ )  
 Coefficient of Thermal Expansion (CTE) of the fiber ( $\alpha_{FIBER}$ )  
 Fiber Volume Fraction (FV)  
 Typical spacing between cracks =  $f(\epsilon_{RESIN}^{ULT}, \alpha_{FIBER}, FV, CPT)$

Material: M55J / 934  
 Ply Thickness: 4.5 mils (114 microns)  
 Fiber Volume Fraction: 59%

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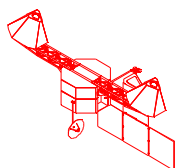




# Microcracking Performance of Space Composites



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Resin System	Ply Thickness (MILS)	Cracks/Inch (After No. of Cycles)			
		0 Cycles	10 Cycles	50 Cycles	100 Cycles
934	5.0	3.0	33.0	53.5	56.0
954-3	5.0	0.5	4.0	6.5	10.0
934	2.5	0	2.0	2.5	3.0
954-3	2.5	0	0	0	0

## Notes:

1. P-75 laminates, (45, 0, -45, 90)<sub>3S</sub>, 60% FV, 2 in. x 2 in.
2. Cycle: -- 150° F to +150 ° F and back @ 20° F/min., 5 min. dwell at extremes.
3. Data taken at 50x magnification; values are average of 0 ° normal and 90 ° normal edges.

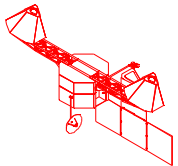


## Proposed Microcracking Experiments

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- **Create Laminates Which Will Microcrack**
  - M55J, (0,90)XS or (0,45,90,135)XS
  - Cyanate and epoxy resins
- **Monitor During Thermal Cycles (to 196 K, ~ 20 cycles)**
  - CU Microdynamics Lab, or
  - Adapt COI Liquid Helium CTE facility
  - Acoustic emission measured
  - Dynamic response measured
- **Characterize:**
  - Frequencies
  - Energy, amplitude
  - Internal composite damping for microcracking input